



# Validation of CFD models to predict hydrodynamics of stirred tank flows in the transitional flow regime.

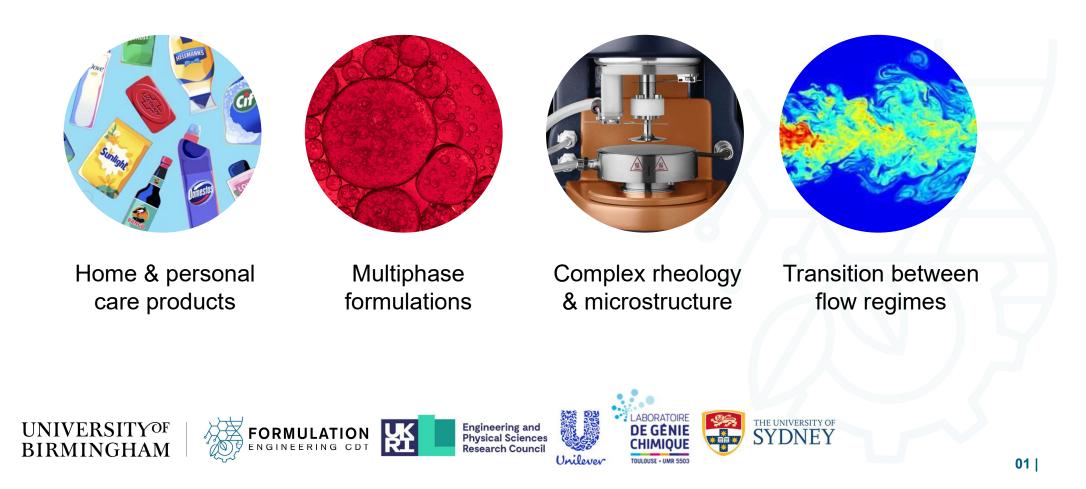
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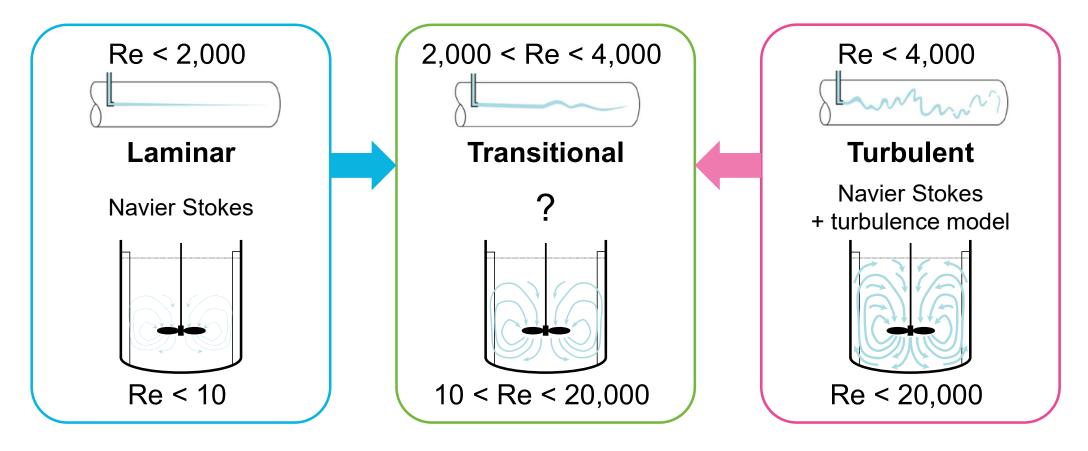
#### IChemE Fluid Mixing Processes Meeting 10<sup>th</sup> January 2024

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#### **Project Context**

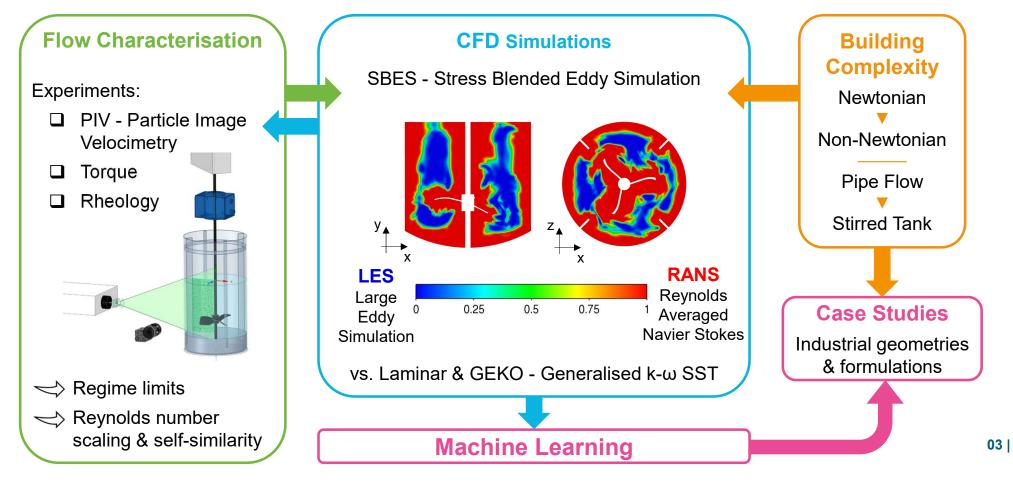


#### **State of the Art - Modelling of Transitional Flows**



## **Aims - Investigative Approach**

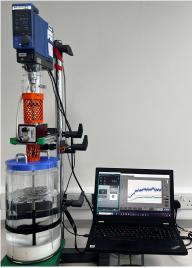
#### "Prediction of complex industrial flows in the transitional regime"



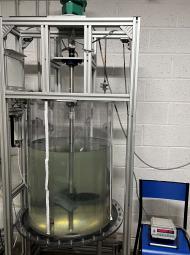
#### overhead motor torque sensor (20 - 550 rpm) PIV 5 L (0.225 - 1 Nm)Impeller shaft glass tank (d<sub>s</sub> - 8 mm) (d<sub>t</sub> - 190 mm) 3 mm thick acrylic baffles Fluorescent $(w - d_t/10)$ polymer particles (1-20 µm) fill level (dt) A320 hydrofoil impeller $(d_{i} - d_{t}/2, OB - d_{t}/3)$ Nd-Yag Laser hard resin dish-(523 nm, 10Hz) bottomed tank insert 4MP-HS CCD camera (2048 x 2048 pixels<sup>2</sup>)

**Experimental Set-Up** 

Torque 5 L

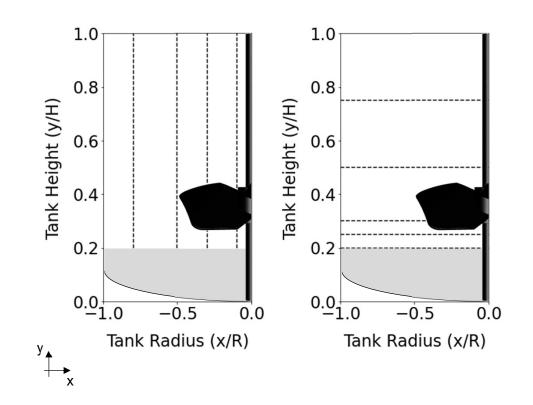


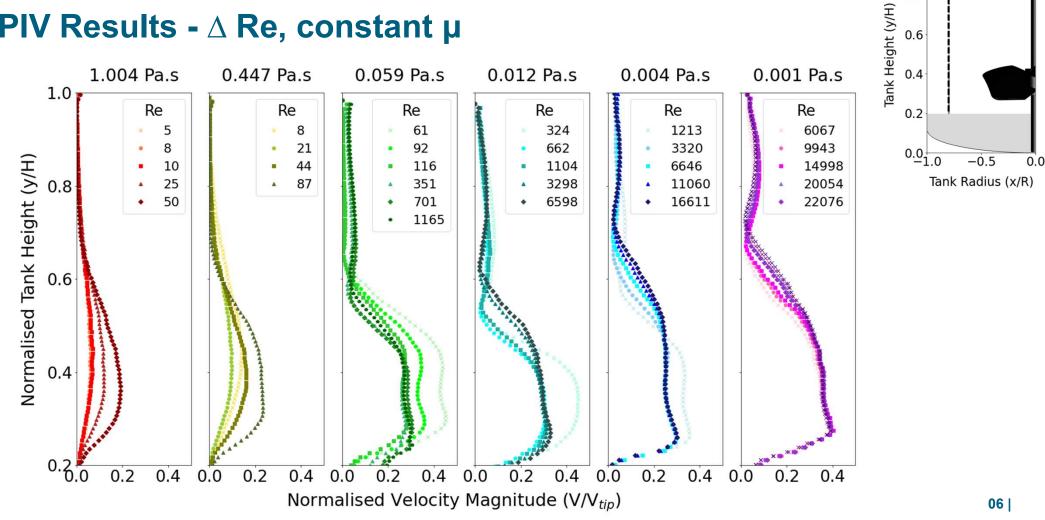
Torque 170 L



#### **Stirred Tank Investigation – PIV & Torque**

- □ **Re** = 5 35,000
  - □ V<sub>tip</sub> 0.1 2.7 m/s
  - □ µ (apparent) 1.5 0.001 Pa.s
    - □ Glycerol (40 100 wt%)
    - □ CMC (0.1 0.2 wt%)
- Observe trends of normalised velocity magnitude & fluctuations
  - $\hfill \Delta$  Re, constant  $\mu$
  - $\hfill \Delta$   $\mu,$  constant Re
  - Newtonian vs non-Newtonian





-0.8R

1.0

0.8

0.6

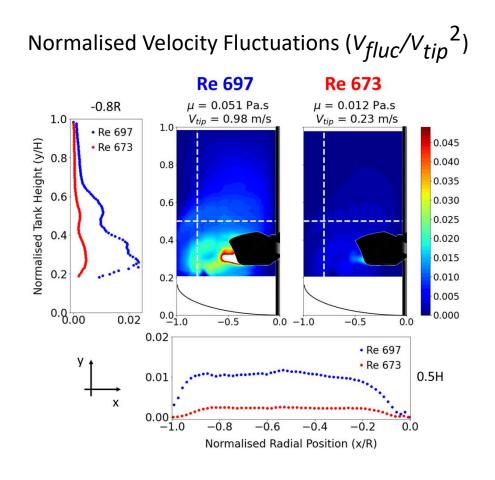
## **PIV Results -** $\triangle$ **Re, constant** $\mu$

#### **PIV Results -** $\Delta$ µ, constant Re

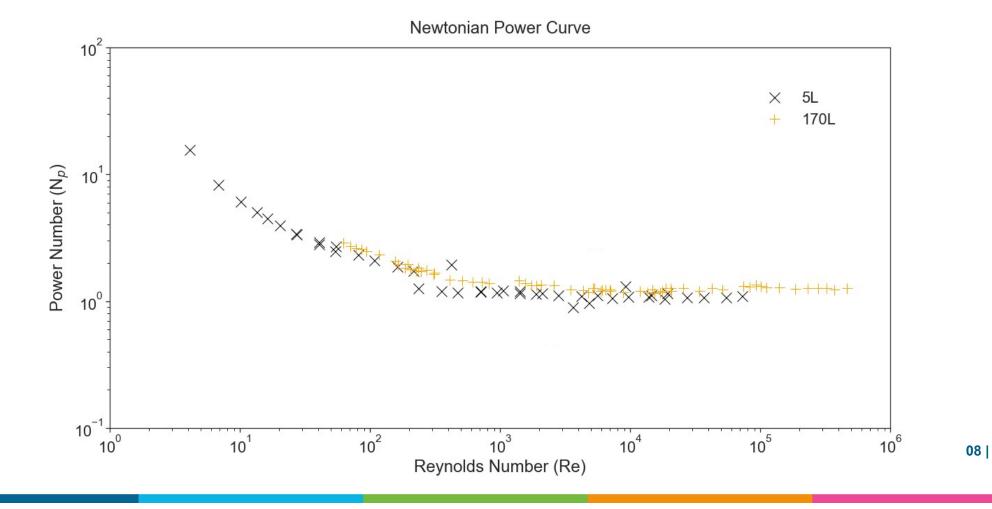
Normalised Velocity Magnitude (V/V<sub>tip</sub>)

Re 697 Re 673  $\mu = 0.051 \text{ Pa.s}$  $\mu = 0.012 \text{ Pa.s}$ -0.8R  $V_{tip} = 0.98 \text{ m/s}$  $V_{tip} = 0.23 \text{ m/s}$ 1.0 1.0 0.40 • Re 697 Normalised Tank Height (y/H) • Re 673 0.35 0.8 0.8 0.30 0.25 0.6 0.6 0.20 0.4 0.4 0.15 0.10 0.2 0.2 0.05 0.0<sup>1</sup>0.0 0.1 0.2 0.3 0.0 0.00 -0.5 0.0 -1.0 -0.5 0.0 0.3 • Re 697 y 0.2 • Re 673 ..... 0.5H 0.1 х 0.0 -0.8-0.6-0.4-0.20.0 Normalised Radial Position (x/R)

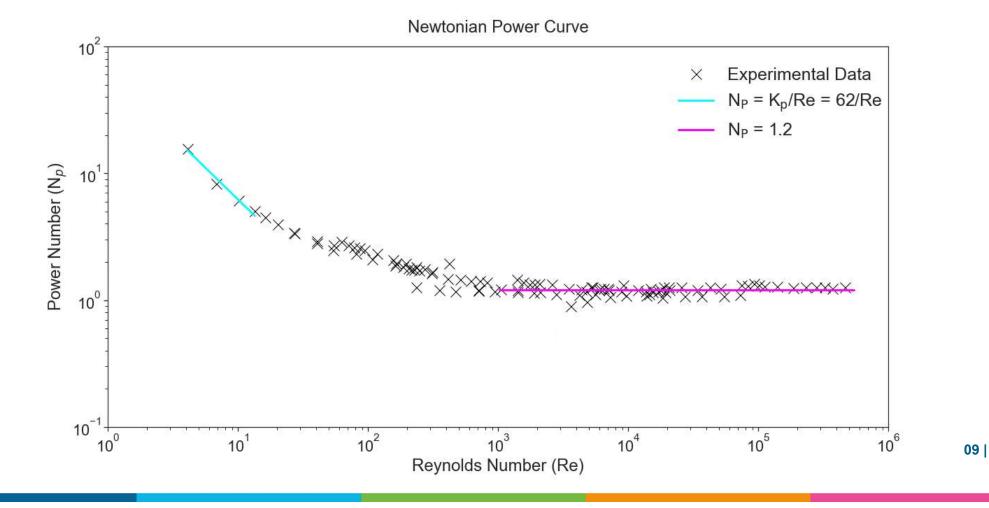
 $V_{fluc} = \frac{3}{4}\sqrt{\tilde{u}^2 + \tilde{v}^2}$ 



#### **Torque Results – 5L vs 170 L**



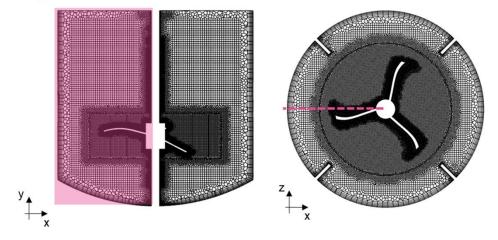
#### **Torque Results – Laminar & Turbulent Regime Fitting**

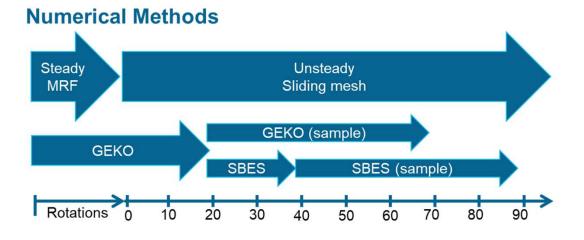


#### **Simulation Set-up**

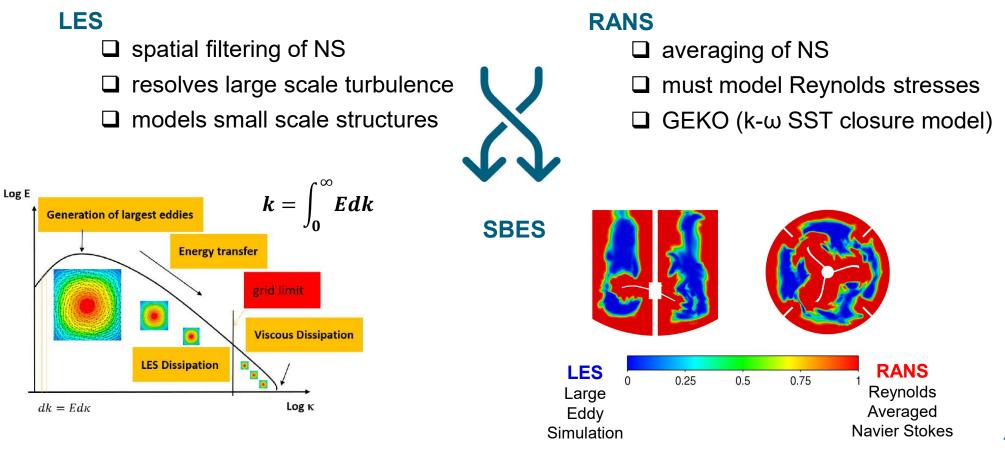
- □ Convergence monitors
  - **\Box** Residual values <  $10^{-6}$
  - □ Torque (impeller & walls)
  - $\Box \quad \text{Mass integral of } \varepsilon$
- Data sampling on a fixed plane
  - All blade positions
  - Periodic (every full rotation) estimate pseudo turbulence due
    to blade contributions.

#### Polyhexcore mesh - 2.14M cells





## Scale Resolving Simulations – Why SBES?

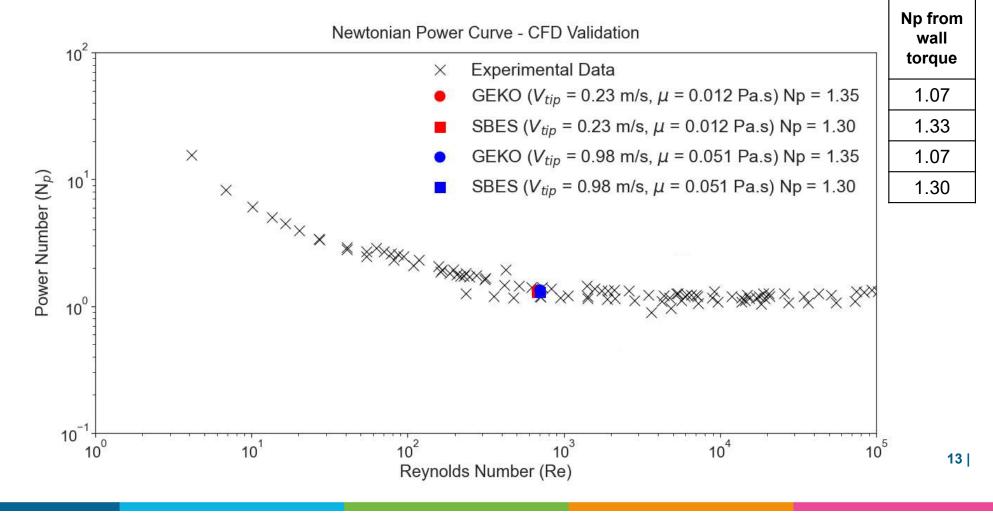


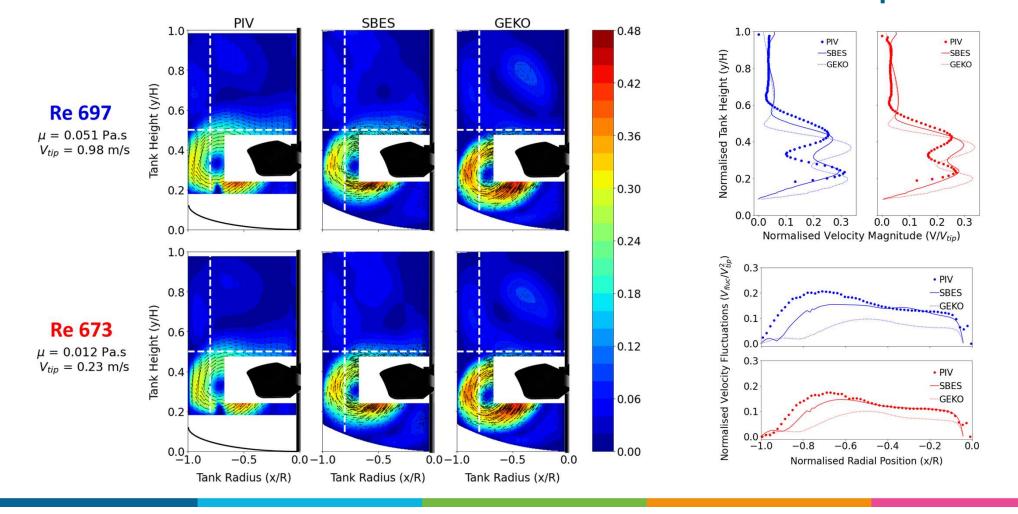
Menter, F., (ANSYS), Best Practice: Scale-Resolving Simulations in ANSYS CFD. 2015.

#### Blending function for SBES Wall Y+ **Cell Convective Courant** (LES = 0, RANS = 1) 0.0 0.5 1.0 1.5 2.0 0.0 0.5 1.0 1.5 2.0 0.0 0.2 0.4 0.6 0.8 1.0 **?**-8

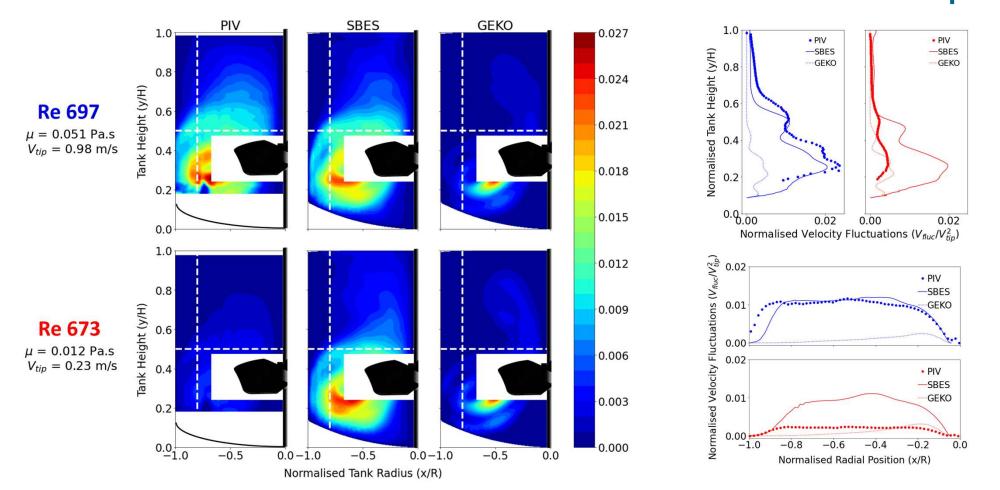
## **Simulation Solution Checks**

#### **CFD Validation - Torque**





# **CFD Validation – Normalised Velocity Magnitude (V/V<sub>tip</sub>)**



# CFD Validation – Normalised Velocity Fluctuations (V<sub>fluc</sub>/V<sub>tip</sub><sup>2</sup>)

## Conclusions

- Distinct flow behaviours identified for each flow regime.
- $\Box$  Transitional regime limits are not constant vary with fluid viscosity ( $\mu$ ).
- Transitional regime flows scaled for same Re do not exhibit self-similar flow hydrodynamics.
- Both GEKO & SBES closure models validated for torque prediction.
- □ SBES performs better to predict torque balance & velocity magnitudes.
- **G** Failure to predict difference in velocity fluctuations between two transitional regime cases with same Re.

#### **Future Work**

- □ Fix SBES blending function to run larger region of LES.
- □ Confirm both GEKO & SBES accurately predict high Re cases.
- Explore impeller blade and baffle periodicity using POD & periodic averaging.







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