

# Biodiesel production using liquid – liquid film reactors

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UNIVERSIDAD  
**NACIONAL**  
DE COLOMBIA



## Research questions

Is it possible to produce biodiesel using liquid – liquid film reactors?

If it is possible, is the productivity higher than the obtained in typical industrial process, where CSTR are used implementing three or more reaction-separation stages?

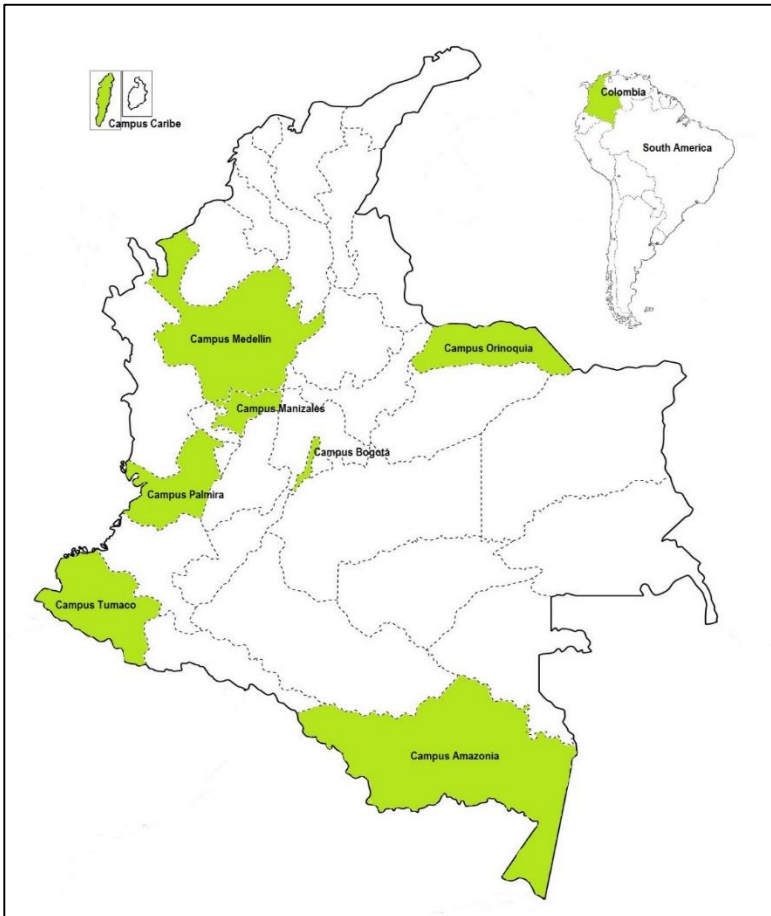


## Outline

- Universidad Nacional de Colombia
- Biodiesel production in Colombia
- Falling Film Contactors
- Co-current operation
- Counter-current operation
- Co-current integrated with hollow fiber membrane (HFM)
- Conclusion



# Universidad Nacional de Colombia



8

Campus

52,550

Students

94

Undergraduate  
programs

361

Graduate programs



# School of Engineering

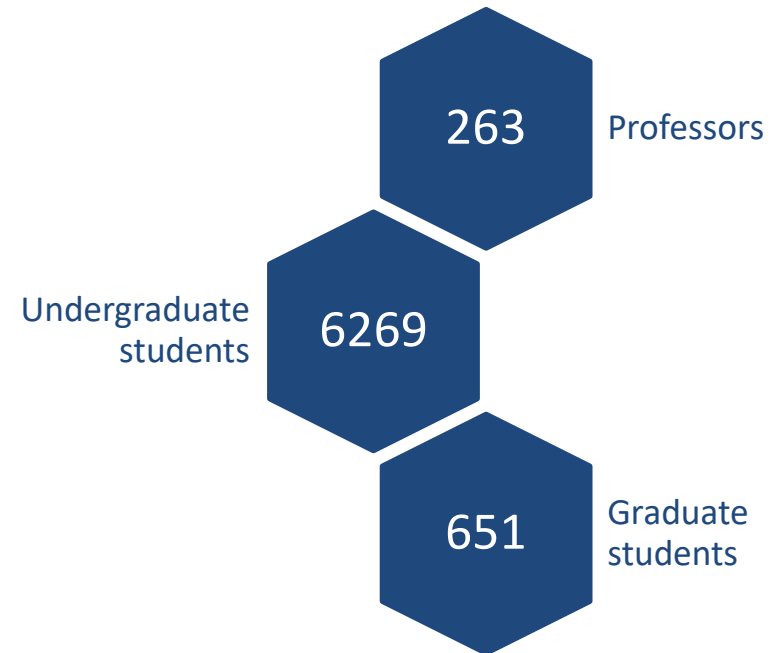
Civil and Agriculture

Chemical and Environmental

Electric and Electronics

Mechanical and Mechatronics

Systems and Industrial





## Palm oil production in Colombia

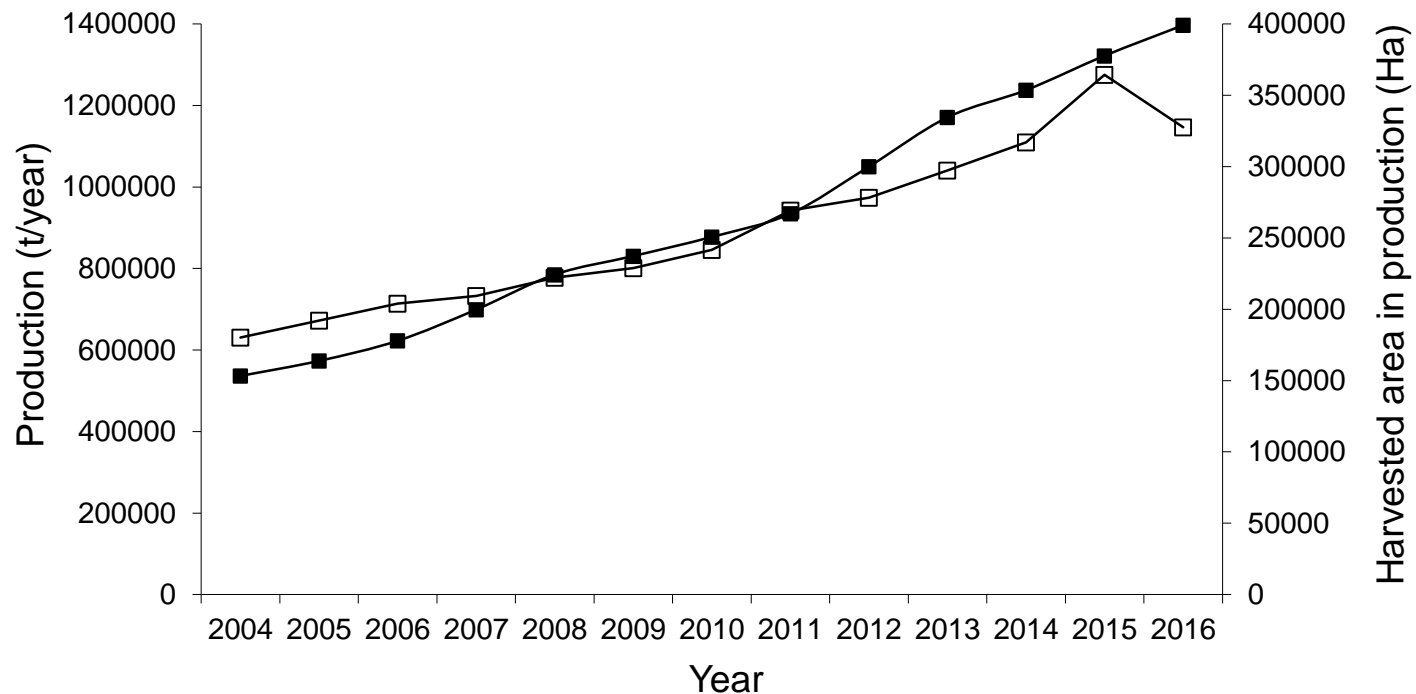


Figure 1. Oil palm harvested area in production (□) and palm oil production (■)

Data from <http://www.fedebiocombustibles.com/nota-web-id-488.htm>, retrieved July 2018



## Biodiesel production

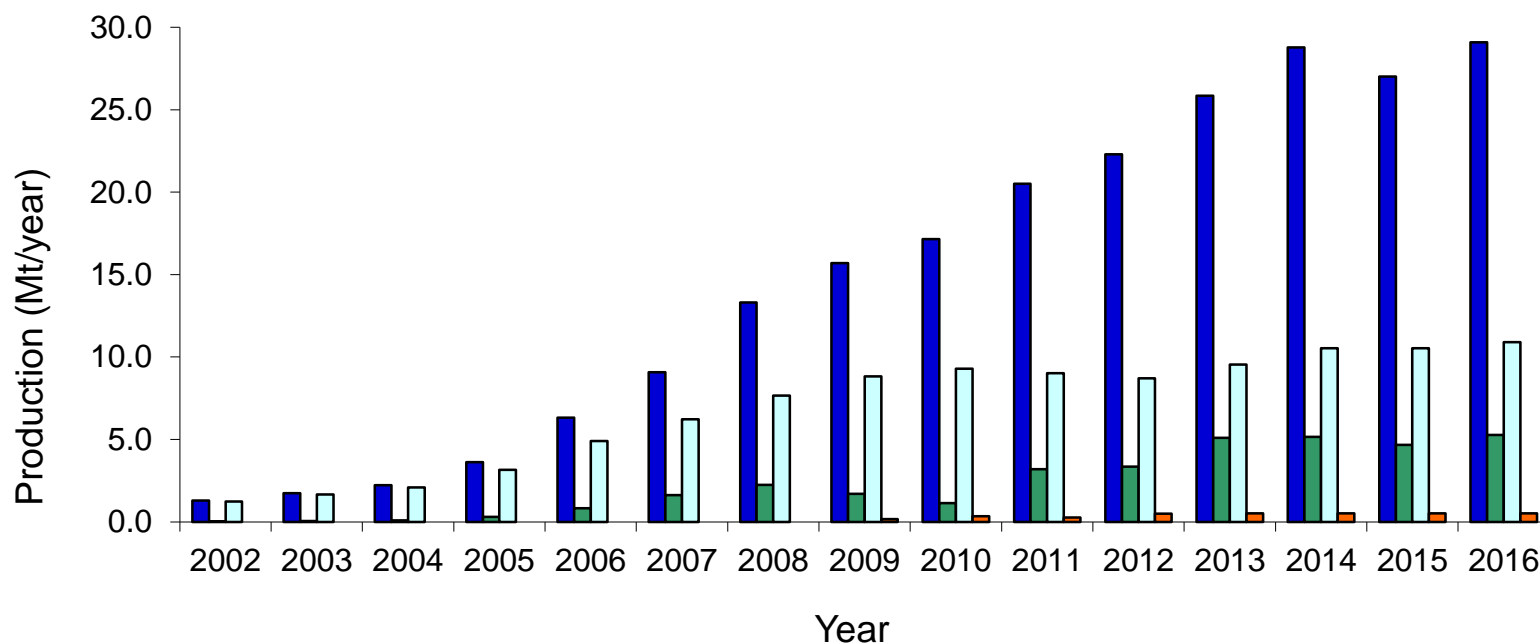


Figure 2. Biodiesel production (■) World (■) United States (■) European Union (■) Colombia

Data from <http://www.eia.gov/cfapps/ipdbproject>, retrieved July 2017



## Biodiesel production in Colombia

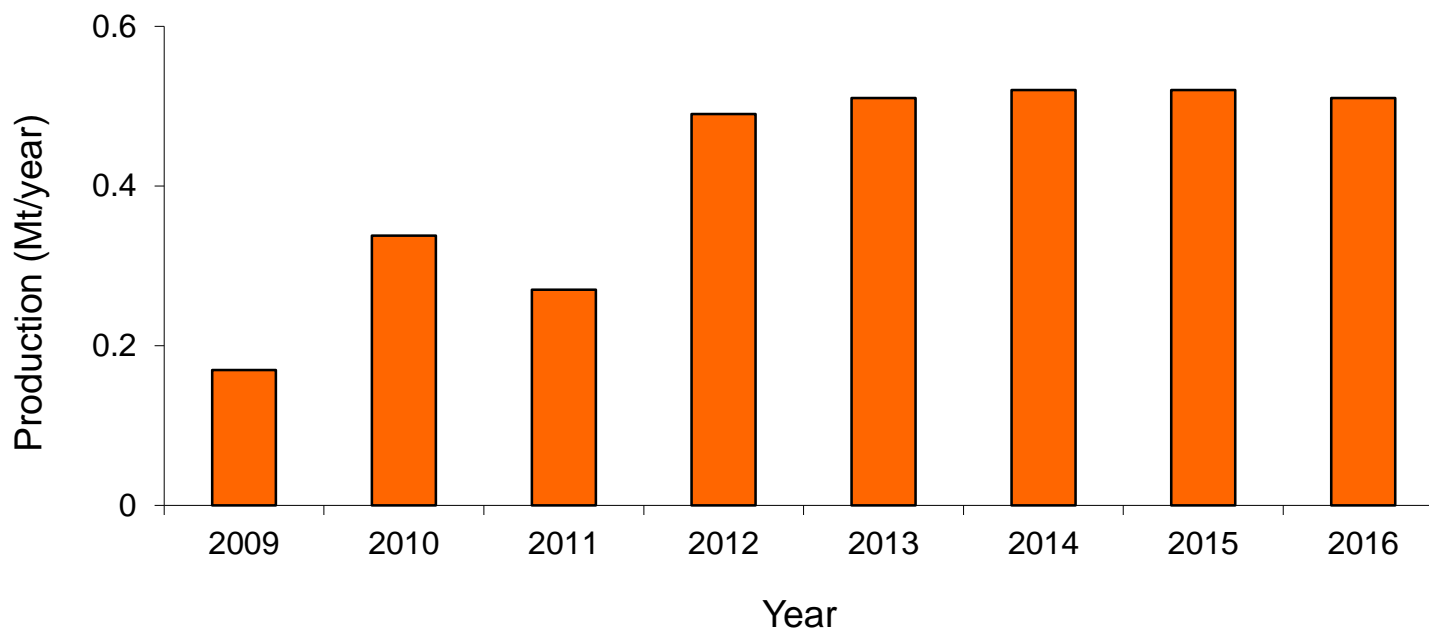


Figure 3. Biodiesel production in Colombia (0.5 Mt/year)

Data from <http://www.fedebiocombustibles.com/nota-web-id-488.htm>, retrieved July 2018





## Why did we propose the use LLFC in biodiesel production?

- To promote the contact of two phases (ester and alcohol – rich) without dispersing one phase into the other.
- To reduce separation time required in separators (decanter) downstream the reactor.
- To increase conversion and yield by simultaneous extraction of glycerol produced during transesterification reaction.

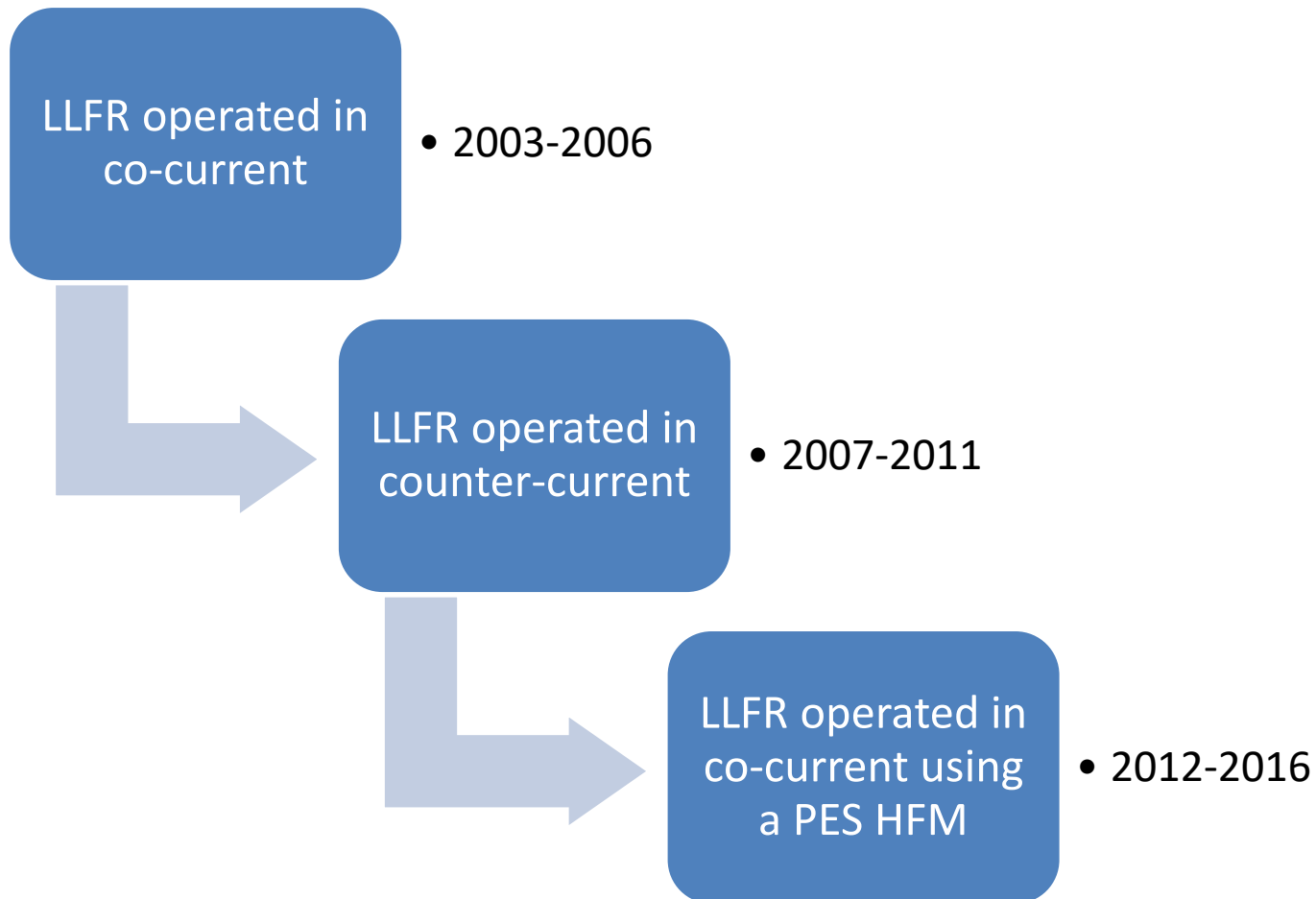


## Why use LLFC in biodiesel production?

- Because biodiesel production is mainly a heterogeneous reaction requiring dispersion of alcohol rich phase into ester rich-phase
- Because smaller the droplet size higher the residence time in decanters and higher energy consumption
- Because chemical equilibria limit biodiesel yield. Thus several reaction stages are required to accomplish glycerol free and bonded specification

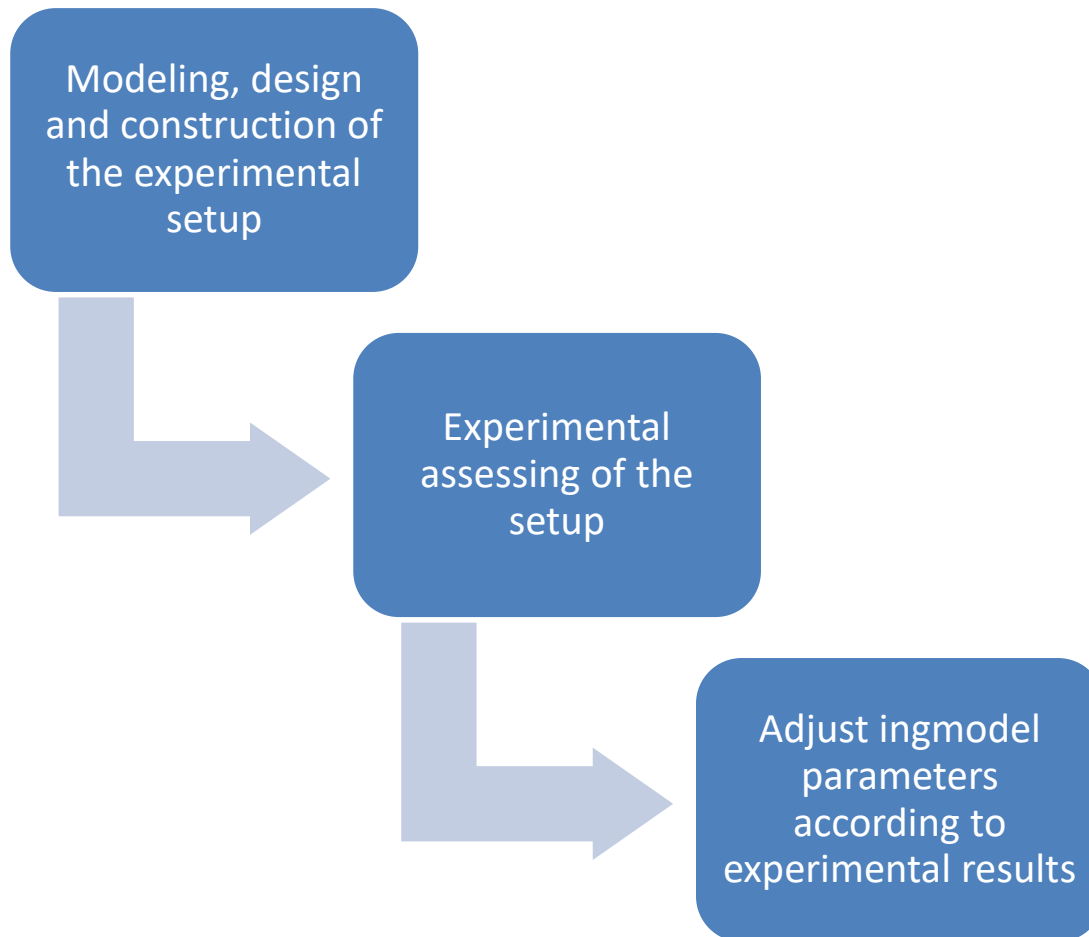


## Technologies assessed





# General methodology





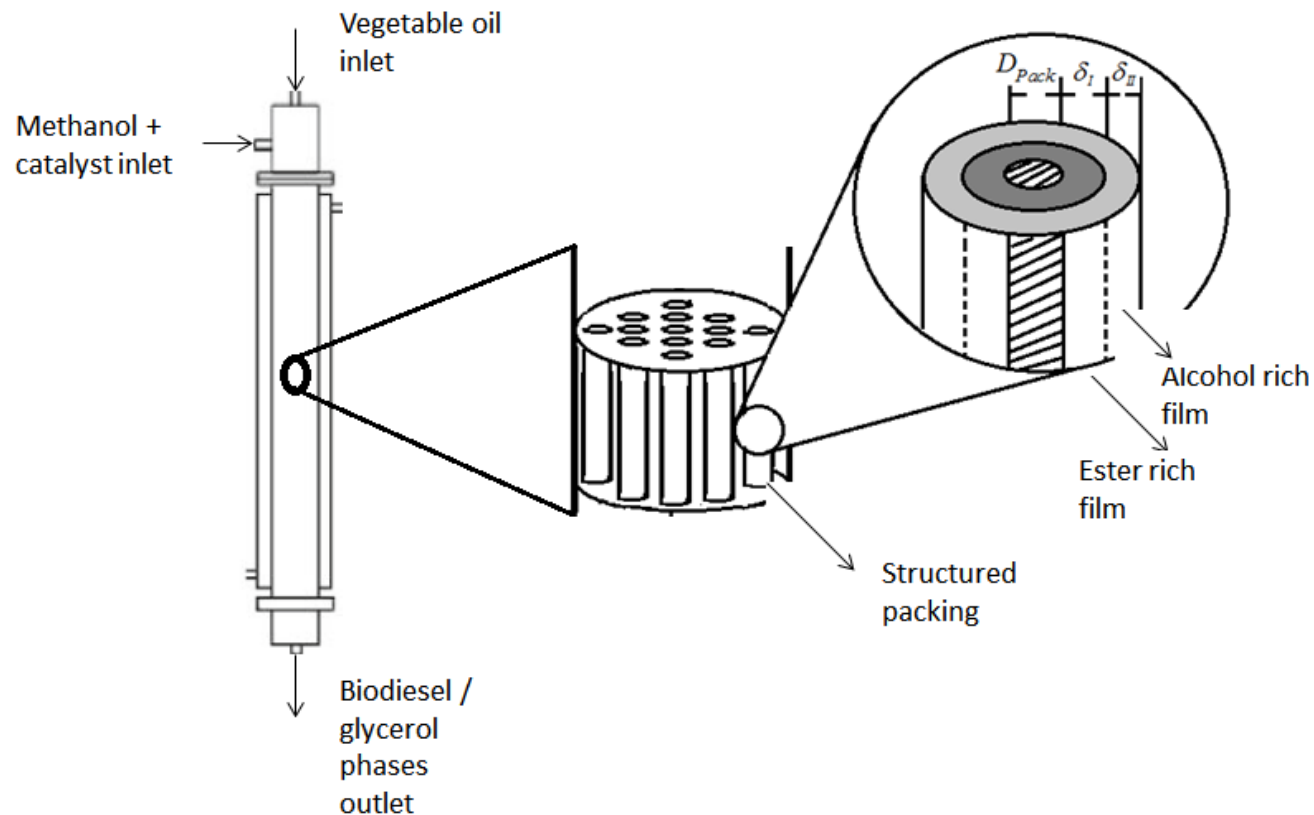
## What is going to be kept constant?

The catalyst: sodium methoxide

The alcohol: methanol

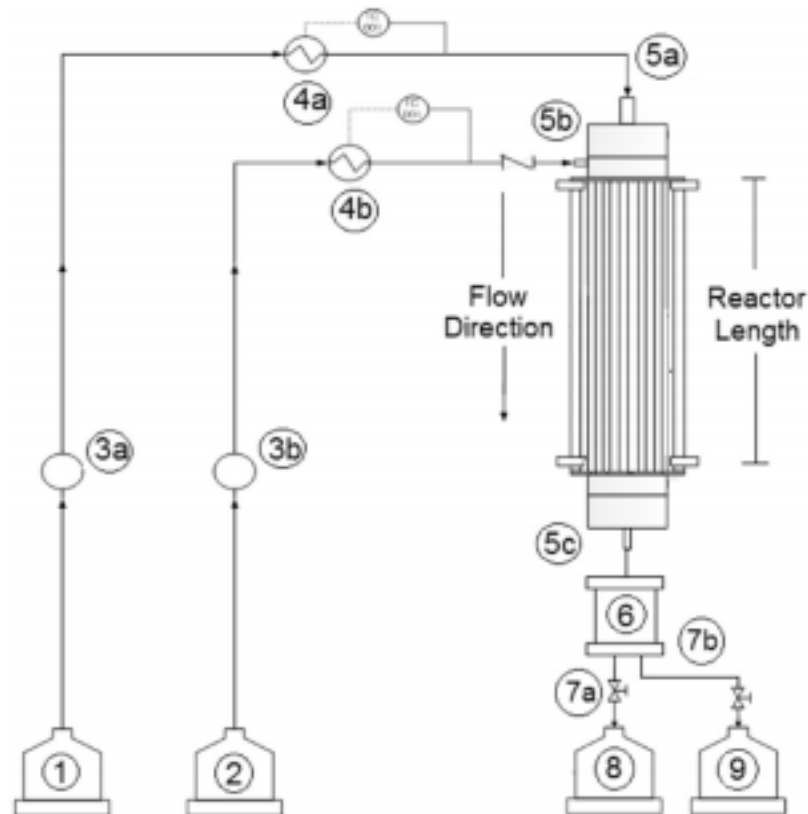


# Biodiesel production in LLFR operated in co-current



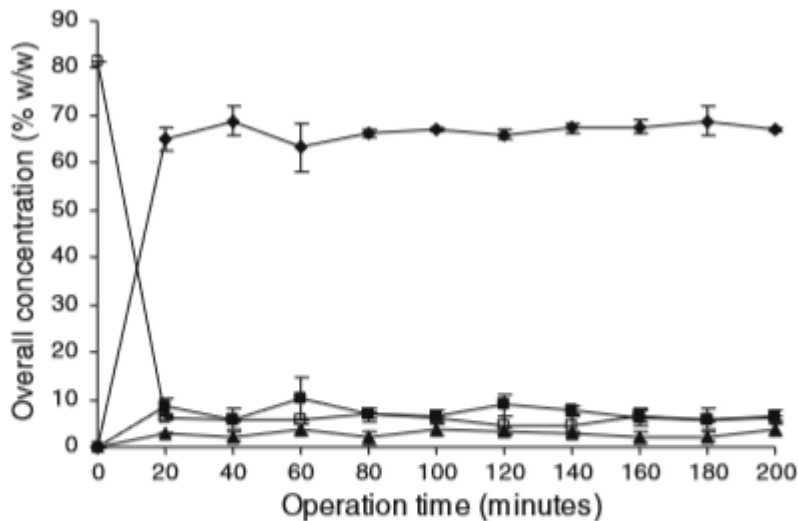


## Biodiesel production in LLFR operated in co-current

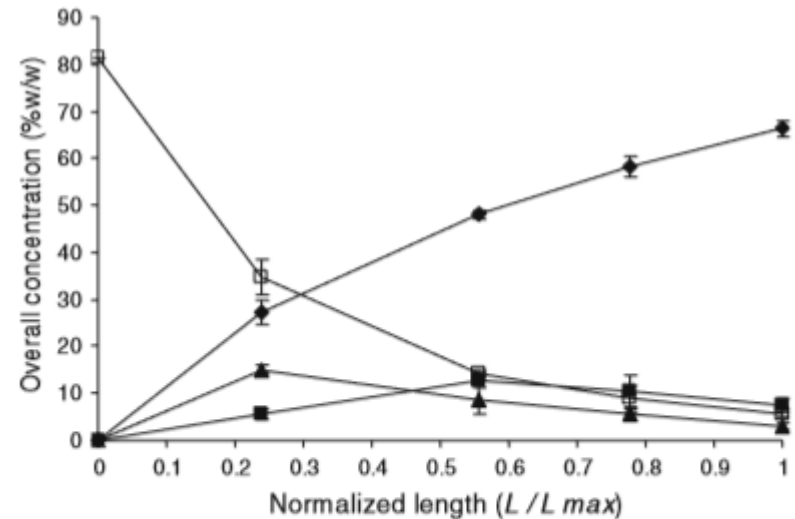




## Biodiesel production in LLFR operated in co-current



**Fig. 3** Overall concentration of palm oil, methyl esters, monoglycerides and diglycerides at the outlet of the LLFR of  $L/L_{max}$  1.0, during the palm oil methanolysis. Palm oil flow rate  $27.0 \text{ g min}^{-1}$ , methanol to oil molar ratio 6:1, temperature  $60^\circ\text{C}$ , 1 wt.% NaOH based on palm oil. (Filled diamond) methyl esters; (filled square) monoglycerides; (filled triangle) diglycerides; (square) palm oil



**Fig. 4** The effect of the LLFR length on the overall concentration of some feedstock and products during palm oil methanolysis. Palm oil flow rate  $27.0 \text{ g min}^{-1}$ , methanol to oil molar ratio 6:1, temperature  $60^\circ\text{C}$ , 1 wt.% NaOH based on palm oil. (Filled diamond) methyl esters; (filled square) monoglycerides; (filled square) diglycerides; (square) palm oil. Experimental data correspond to the steady state behavior of the reactor





# Biodiesel production in LLFR operated in co-current

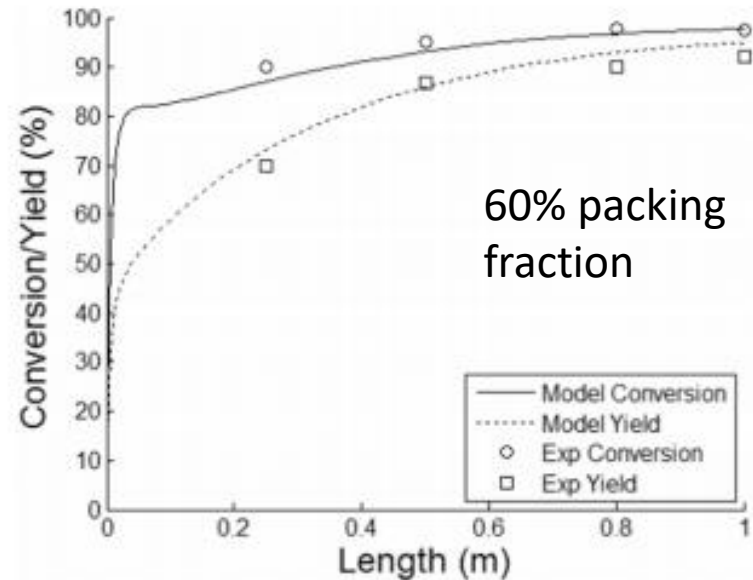
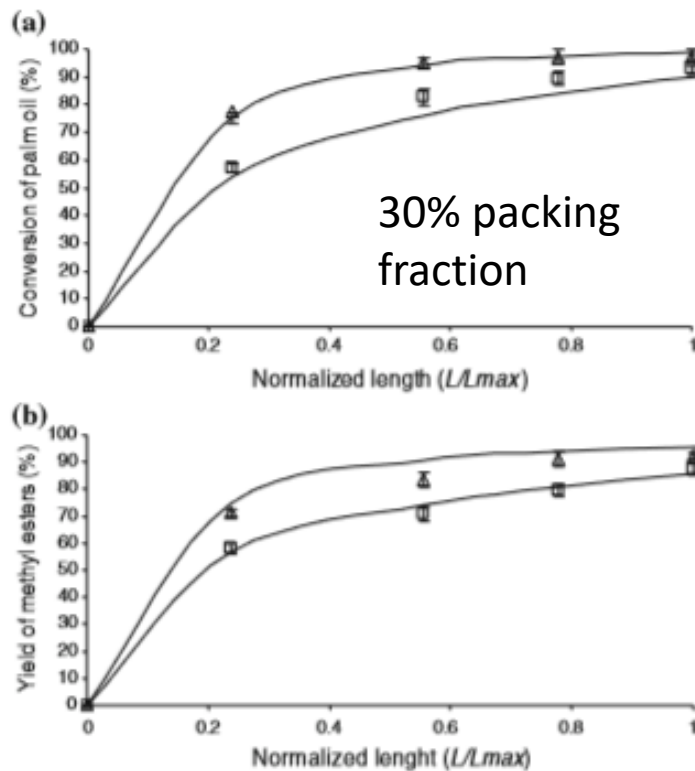


Fig. 10. Reactor length effect on the conversion and FAME yield. VO flow rate  $40 \text{ g min}^{-1}$  and  $a_c$  of  $5333 \text{ m}^{-1}$ .

# Biodiesel production in LLFR operated in co-current increasing packing fraction

**Table 4**

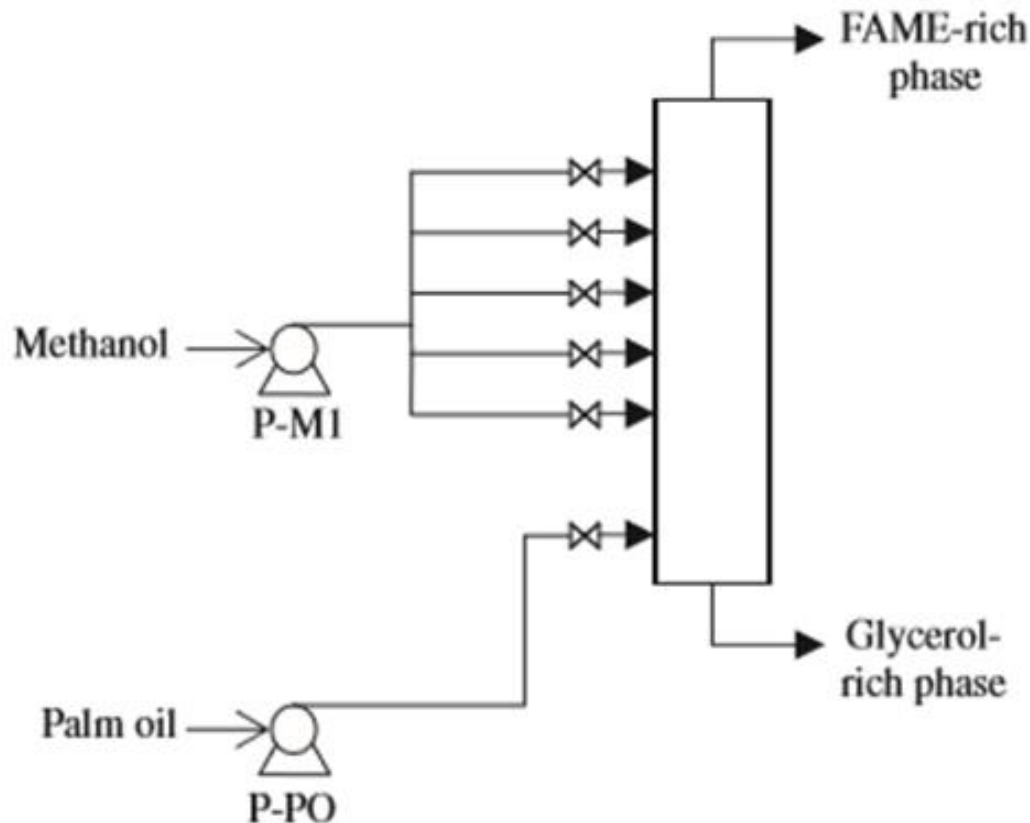
Productivity of biodiesel from soybean oil obtained for LLFR and for BSTR at 55 °C, using NaOH as catalyst (1%wt.).

Variable	BSTR [31]	LLFR [30]	LLFR (this work)	LLFR with decanter (this work)
Conversion (%)	99.9	97.5	99.5	99.9
Yield (%)	97.1	92.2	95.1	97.2
Productivity $\left( \frac{m^3 FAME}{h \cdot m^3 reactor} \right)$	0.3	1.2	3.5	2.5
Flow rate (g/min)	N.A. <sup>a</sup>	9	40	40
Packing surface to volume ( $a_c, m^{-1}$ )	N.A. <sup>a</sup>	444	5333	5333

<sup>a</sup> Not applicable.

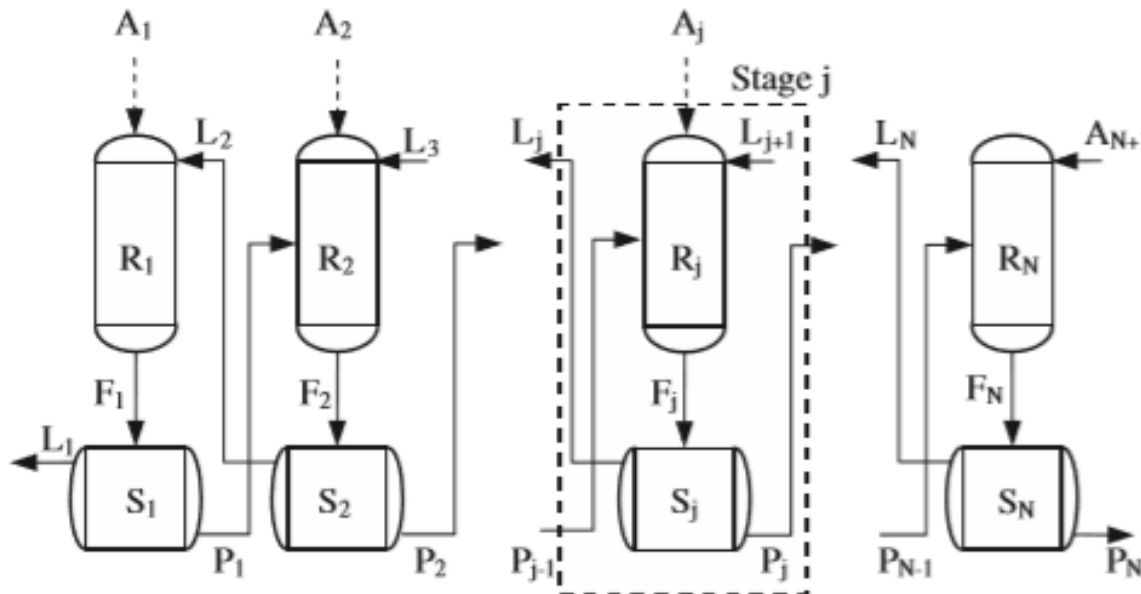


# Biodiesel production in LLFR operated in counter-current



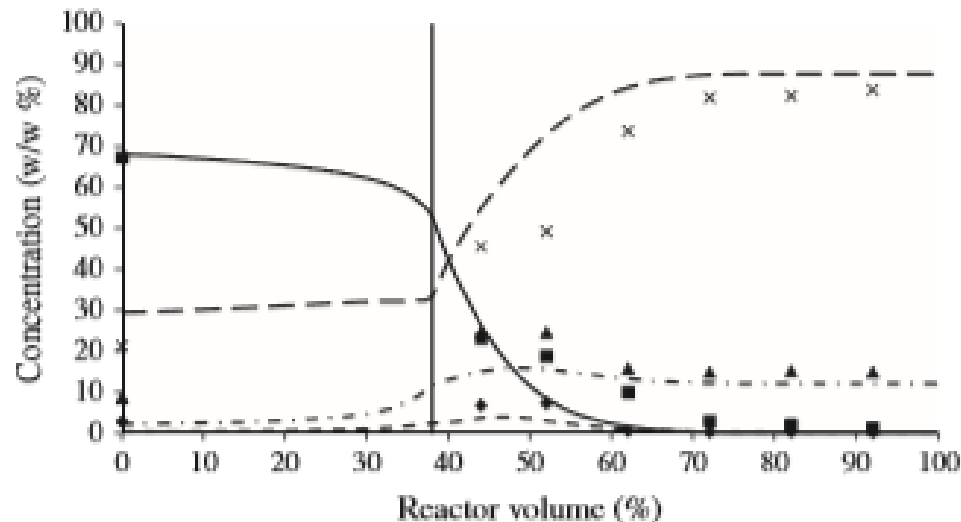


# Biodiesel production in LLFR operated in counter-current





# Biodiesel production in LLFR operated in counter-current



**Fig. 5.** Biodiesel-rich phase experimental and predicted concentrations during biodiesel production using reactive extraction. Palm oil mass flow rate  $32.9 \text{ g min}^{-1}$ , methanol to palm oil molar ratio 3.7, methanol feeding length 38% (vertical line). Experimental data: (■) FAME, (◆) MG, (▲) DG, (×) TG. Model predictions: (—) FAME, (---) MG, (.....) DG, (-.-.-) TG.



## Biodiesel production in LLFR operated in counter-current

**Table 6**

Comparison of productivity between counter-current, co-current and batch processes at 60 °C, using NaOH as catalyst (1 wt.% based on palm oil weight or mass flow rate).

Variable	Process		
	Counter-current	Co-current	Batch
Palm oil mass flow rate (g min <sup>-1</sup> )	50	50	50 <sup>a</sup>
Methanol to palm oil molar ratio	8:1	10:1	12:1
Palm oil conversion (%)	99.7	99.4	99.9
Yield to FAME (%)	99.9	97.2	98.3
Productivity (m <sup>3</sup> of FAME m <sup>-3</sup> h <sup>-1</sup> )	1.8	1.2	0.3

<sup>a</sup> In this case the variables are palm oil mass and reaction time. The reactor volume is evaluated from the reaction mass.

## Biodiesel production in LLFR operated in co-current and hollow fiber membranes

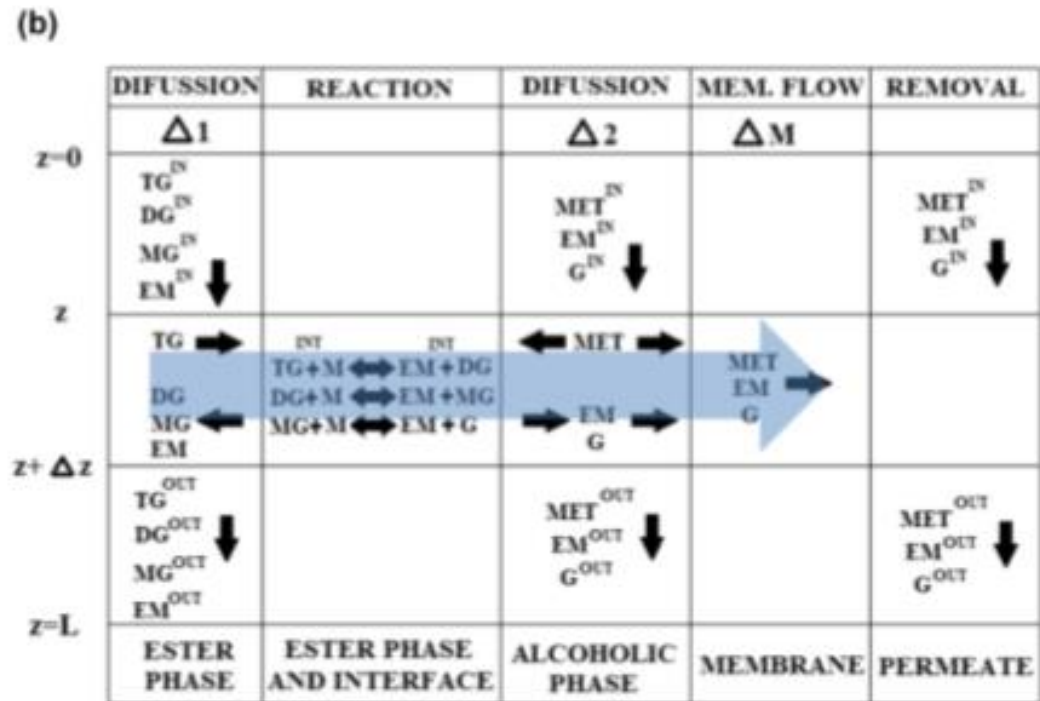
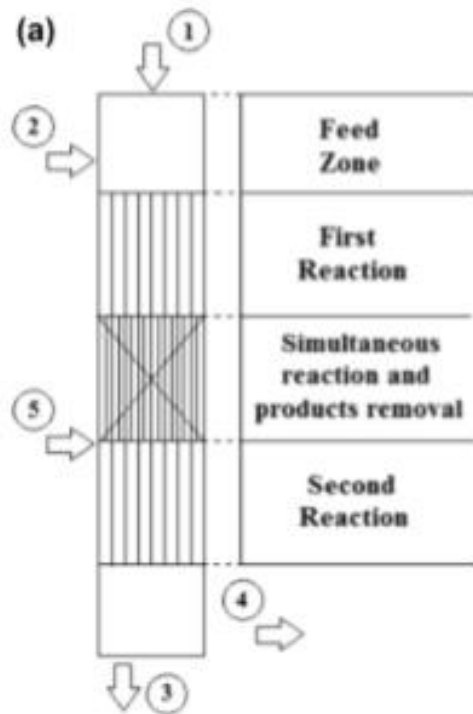
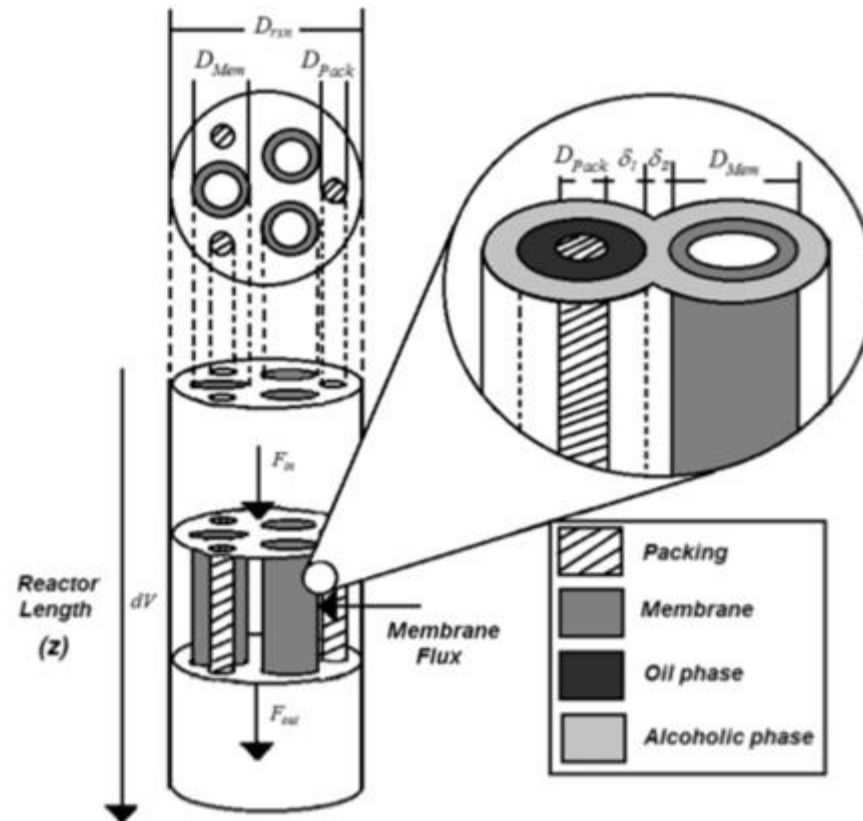


Fig. 1. a) Schematic representation of the LLFRM. b) Schematic transport model in the LLFRM.



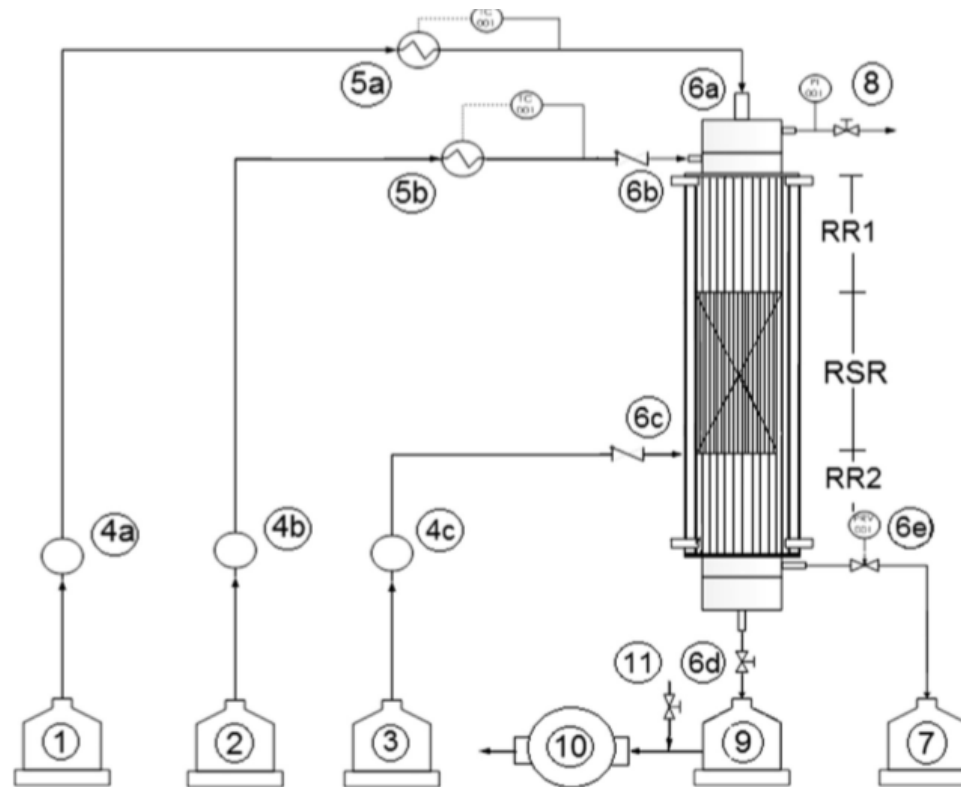
## Biodiesel production in LLFR operated in co-current and hollow fiber membranes







## Biodiesel production in LLFR operated in co-current and hollow fiber membranes





## Biodiesel production in LLFR operated in co-current and hollow fiber membranes

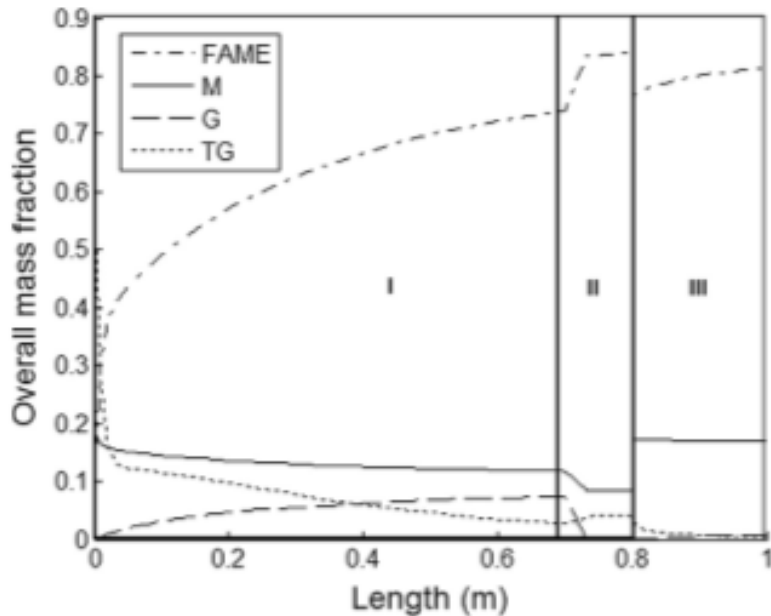


Fig. 6. Performance of the LLFRM over the reactor length as predicted by the model. Temperature 55 °C, Catalyst concentration 1%wt, VO flow rate 20 g min<sup>-1</sup>, 9:1 methanol to oil molar ratio and 33% Lateral methanol.

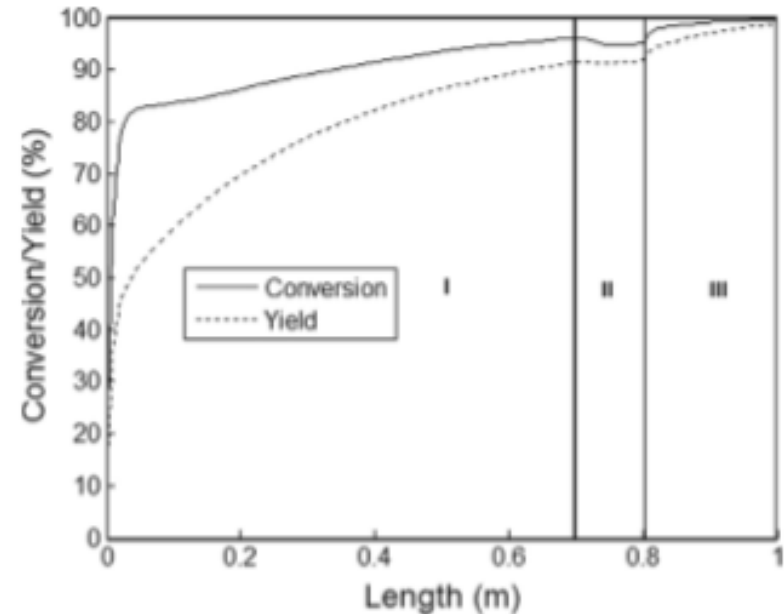


Fig. 7. Model prediction of conversion and FAME yield in an LLFRM. Temperature 55 °C, Catalyst concentration 1%wt, VO flow rate 20 g min<sup>-1</sup>, 9:1 methanol to oil molar ratio and 33% Lateral methanol [46].



## Biodiesel production in LLFR operated in co-current and hollow fiber membranes

**Table 4**

Productivity of biodiesel from soybean oil obtained for LLFR, LLFRM, and CSTR at 55 °C, using NaOH as catalyst (1%wt).

Variable	CSTR	LLFR with decanter [47]	LLFR [47]	LLFRM (This work)
Conversion (%)	99.9	99.5	99.9	99.7
Yield (%)	97.1	95.1	97.2	99.3
Productivity $\left( \frac{m^3_{FAME}}{h \cdot m^3_{reactor}} \right)$	0.35	3.5	2.5	3.5
Required Stages	2	1	1	1



## Conclusion

It is possible to produce biodiesel accomplishing specifications defined in product standards using LLFR operated in two different configurations: counter-current and co-current using HFM implementing only one reaction step, reducing separation time and, as a consequence, increasing process productivity. In co-current two reaction steps are required.

The highest productivity was obtained for the LLFR operated in co-current (with and without membranes).